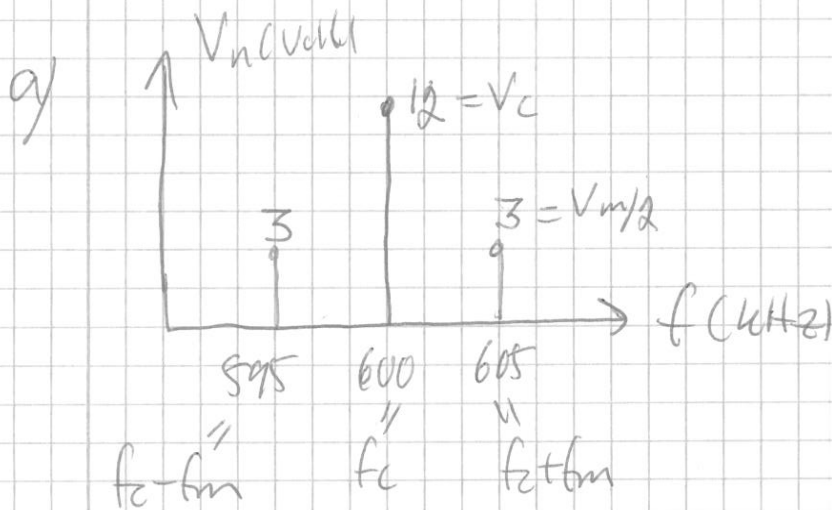


RPY010 Telekomunikationer

18/12-2012

① Se kurslitteratur/föreläsningsteknik/lab. 3

② $V_c = 12\text{ V}$, $f_c = 600\text{ kHz}$, $V_m = 6\text{ V}$, $f_m = 5\text{ kHz}$



b)

$$\frac{V_{eff}^2}{R} = \frac{1}{2R} \left\{ V_c^2 + \left(\frac{V_m}{2}\right)^2 + \left(\frac{V_m}{2}\right)^2 \right\}$$

$$V_{eff} = \sqrt{\frac{1}{2} (12^2 + 3^2 + 3^2)} = \underline{\underline{9\text{ V}}}$$

③ Kretsens övre gren:

Efter 1:a blandaren: $\frac{V_m}{2} \left\{ \cos(\omega_m + \omega_c)t + \underbrace{\cos(\omega_m - \omega_c)t}_{\text{LP-filtreas bär}} \right\}$

Efter 2:a blandaren:

$$\frac{V_m}{4} \left\{ \cos(\omega_c + \omega_m - \omega_c)t + \cos(\omega_c - \omega_m + \omega_c)t \right\}$$

Kretsen nedre gren:

Efter 1:a blandaren $\frac{V_m}{2} \left\{ \underbrace{\sin(\omega_{co} + \omega_m)t + \sin(\omega_{co} - \omega_m)t}_{\text{LP-filtrens bär}} \right\}$

Efter 2:a blandaren $\frac{V_m}{4} \left[\cos(\omega_{ci} - \omega_{co} + \omega_m)t - \cos(\omega_{ci} + \omega_{co} - \omega_m)t \right]$

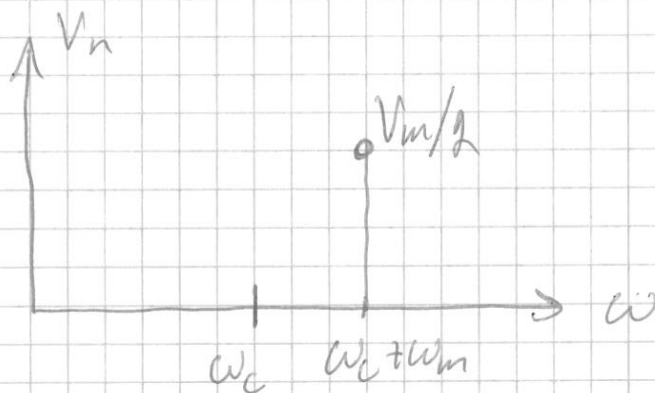
Addera signalerna i båda grenarna:

$$v_{ut} = \frac{V_m}{2} \cos(\omega_{ci} - \omega_{co} + \omega_m)t$$

$\left[\cos(\omega_{ci} + \omega_{co} - \omega_m)t \text{ elimineras} \right]$

Resultatet är alltså en SSB-SC ^{AM-}signal

med bärarfrekv. $\omega_c = \omega_{ci} - \omega_{co}$ och övre
sidbandet kvar.



Modulatorens
implementering
Weavers metod,
se texten
om AM-modulering

$$(4) a) f_i(t) = f_c + \Delta f_c \cdot \cos \omega_m t$$

(fås genom derivering av FM-signalens argument m.a.p. tiden)

$$f_c = \text{frekw. hos spektralkomp. mitt i spektrat} = \underline{\underline{90 \text{ kHz}}}$$

$$f_m = \text{avst. mellan spektralkomp.} = \underline{\underline{8 \text{ kHz}}}$$

$$\Delta f_c = \beta \cdot f_m \Rightarrow \beta \text{ måste bestämmas}$$

Anv. t.ex. komp. $n = 0, 1, 2$

$$2n \cdot J_n = \beta \cdot [J_{n-1} + J_{n+1}]$$

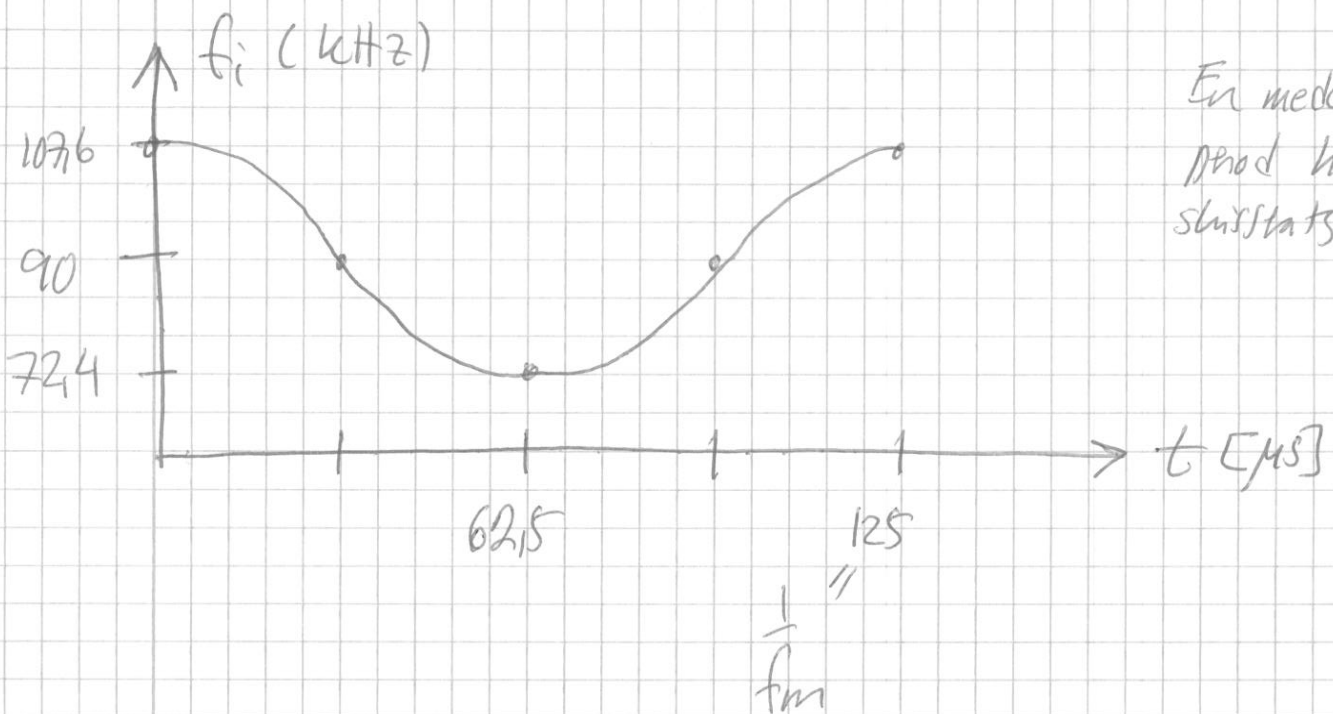
$$\text{Sätt } n=1 \Rightarrow 2 \cdot J_1 = \beta \cdot (J_0 + J_2)$$

$$V_n = V_c \cdot |J_n|, \text{ antag } J_n \text{ positiva} \Rightarrow$$

$$\beta = \frac{2 \cdot V_1}{V_0 + V_2} = \frac{2 \cdot 2,78}{0,552 + 1,975} = 2,2$$

Inspektion i grafer av J_0, J_1 & J_2 i formelbladet $\Rightarrow$
 och $\beta = 2,2$ är alla positiva $\Rightarrow$ OK!

$$\Rightarrow \Delta f_c = 2,2 \cdot 8 = \underline{\underline{17,6 \text{ kHz}}}$$



b) $B \approx 2f_m(1+\beta) = 51.2 \text{ kHz}$

$\Rightarrow$ komponenterna $n=0, \pm 1, \pm 2, \pm 3$ inom B .

$$\frac{P_{\text{inom } B}}{P_{\text{helar}}} = \frac{\frac{1}{2R} \{V_0^2 + 2V_1^2 + 2V_2^2 + 2V_3^2\}}{\frac{1}{2R} V_c^2} =$$

$V_n = V_{-n}$

$$= \frac{V_0^2 + 2V_1^2 + 2V_2^2 + 2V_3^2}{V_1^2 / |J_1|^2} = \frac{0.55^2 + 2 \cdot 2.78^2 + 2 \cdot 1.975^2 + 2 \cdot 0.812^2}{(2.78/0.55)^2}$$

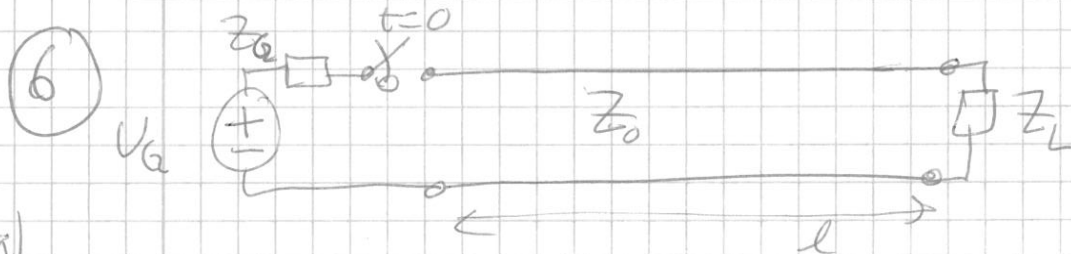
$V_c = \frac{V_1}{|J_1|}$
tex.

$|J_1| \approx 0.55$ ur graf.

≈ 0.974

$\therefore 97.4\%$ av FM-signalens
medel effekt finns inom
Carson bandbredden.

5) Se kurzst. / feldanordnungen.



a)

$$U_G = 12V \quad Z_0 = 75\Omega \quad l = 12m$$

$$Z_G = 50\Omega \quad Z_L = 25\Omega$$

$$\text{Loptiden } \tau = \frac{l}{v_{\text{avg}}} = \frac{12}{3 \cdot 10^8} = 4 \cdot 10^{-8} s = \underline{\underline{40 ns}}$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = -\frac{1}{2}, \quad \Gamma_G = \frac{Z_G - Z_0}{Z_G + Z_0} = -\frac{1}{5}$$

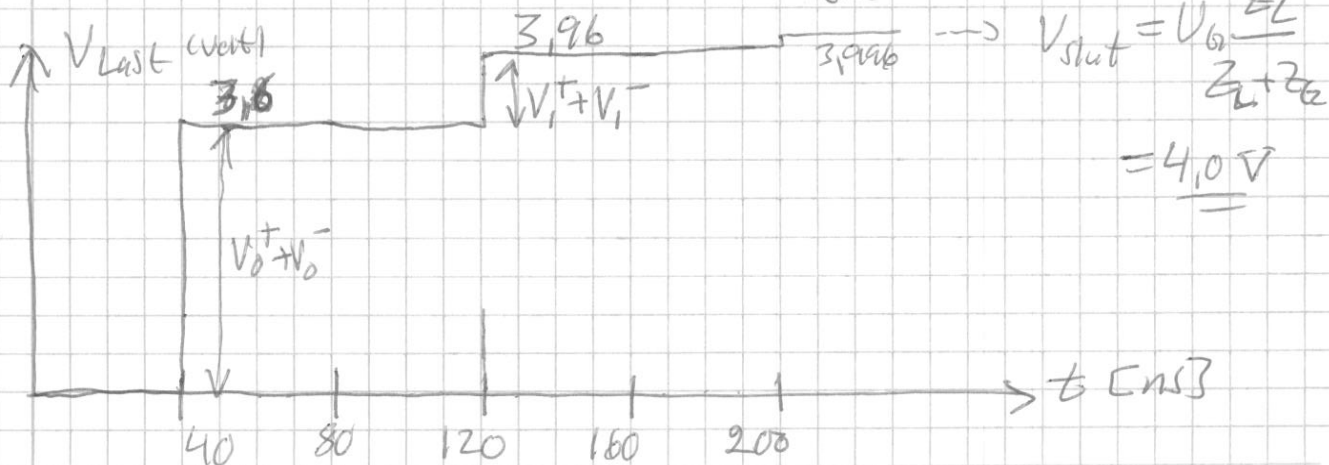
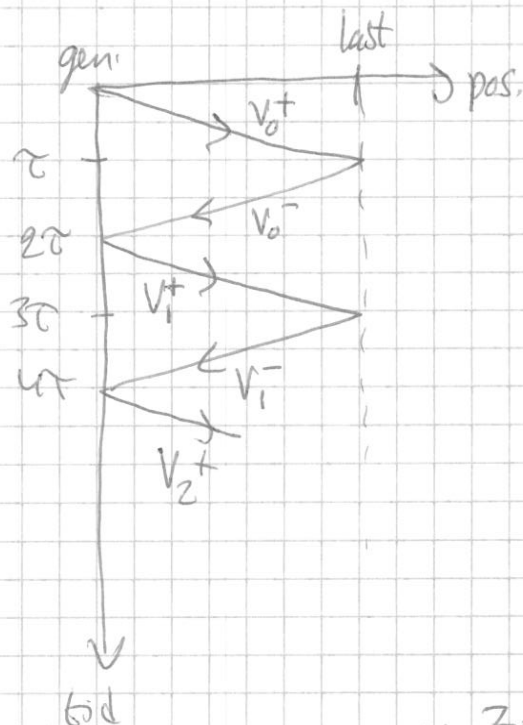
$$V_0^+ = U_G \cdot \frac{Z_0}{Z_0 + Z_G} = \underline{\underline{7.2V}}$$

$$V_0^- = V_0^+ \Gamma_L = -3.6V$$

$$V_1^+ = V_0^- \Gamma_G = +0.72V$$

$$V_1^- = V_1^+ \Gamma_L = -0.36V$$

$$V_2^+ = V_1^- \Gamma_G = +0.072V$$



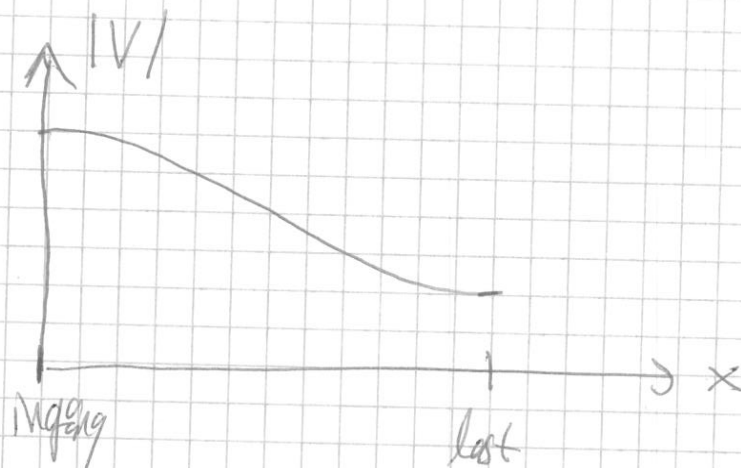
$$b) I_0^+ = \frac{V_0^+}{Z_0} = \frac{7,12}{75} = \underline{\underline{0,096 \text{ A}}}$$

$$c) P_{\text{last}} = \frac{V_L^2}{Z_L} = \frac{V_{\text{stat}}^2}{Z_L} = \frac{4^2}{25} = \underline{\underline{0,64 \text{ W}}}$$

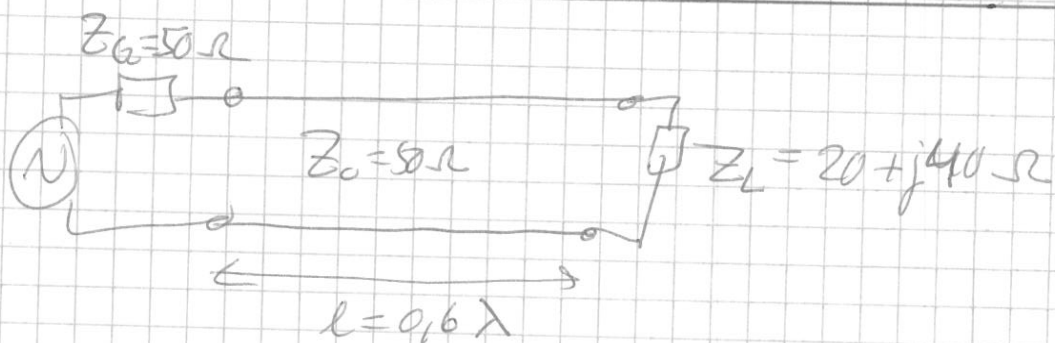
↑
likspänningssignal

$$d) \lambda = 48 \text{ m} \Rightarrow l = 0,25 \lambda$$

$Z_L < Z_0 \Rightarrow P_L < 0 \Rightarrow$ sp. minimum vid last,
ledningslängd $0,25 \lambda \Rightarrow \frac{1}{2}$ vane i SD $\Rightarrow$ sp. max vid
ingången



7



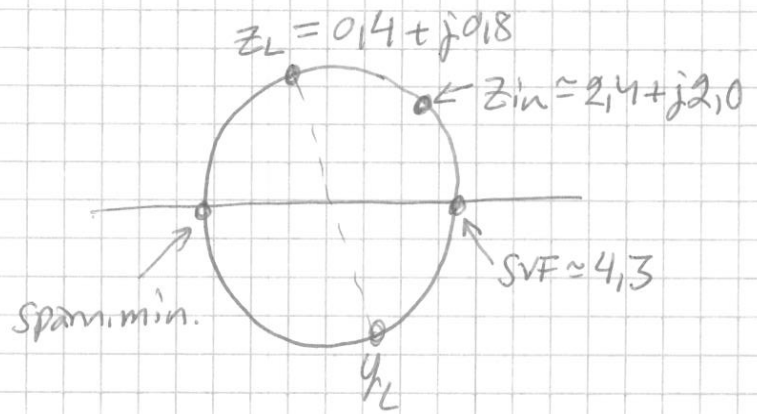
$$\begin{cases} f = 20 \text{ MHz} \\ \omega_{\text{fs}} = 2 \cdot 10^8 \text{ rad/s} \\ \lambda = 10 \text{ m} \end{cases}$$

$$|V^+| = 2,0 \text{ volt}$$

(toppvärde hos våg som infaller
mot lasten)

ab/

Smith diagram:



z_{in} : Går 0.6λ från last mot gen. (medurs)

SWR: skärmpunkt mellan cirkel & realaxel ($z > 1$)

$$\text{Att. bestämma } |\Gamma_L| \Rightarrow SWR = \frac{1 + |\Gamma|}{1 - |\Gamma|} \quad \text{ty } |\Gamma| = |\Gamma_L|$$

$$(|\Gamma_L| \approx 0.620 \Rightarrow SWR \approx 4.27)$$

$$\therefore z_{in} = Z_0 \cdot z_n = 120 + j100 \Omega$$

$$SWR \approx 4.3$$

c) Spann. max inträffa vid skärning med realaxeln ($0 < z < 1$)
 $\Rightarrow$ I vänt från ETT min. 0.384λ ($= 3.84m$) från lasten.

$$|V| = |V^+ + V^-| = |V^+| \cdot |1 + \Gamma| = |V^+| \cdot (1 - |\Gamma|) \approx \underline{\underline{0.76 V}}$$

↑
minimum
 $\Gamma = -|\Gamma|$

d) $\frac{\lambda}{4}$ -transf.: Kopplas in där z reell, t.ex. i 1:a spann. max dvs $\underline{\underline{0.134\lambda}}$ från.

$$Z_{0, \text{transf.}} = \sqrt{Z_{\text{in, kopp.}} \cdot Z_0 Z_0'} = \sqrt{1.3 \cdot 50^2} \approx \underline{\underline{103 \Omega}}$$

Stubbe: Övergår till admittanser $\Rightarrow y_L$, anslut stubben i punkt där $\text{Re } y = 1$, t.ex. $\underline{\underline{0.302\lambda}}$ från lasten
 $y_{\text{in, stubbe}} = -j1.6 \Rightarrow$ stubblängd $\underline{\underline{0.088\lambda}}$