

# Finite-differences in frequency domain

Hand-in assignment # 1 – SSY200

## 1 Problem description

Consider an electromagnetic plane wave that propagates towards a large flat window of glass as shown in Fig. 1. We wish to compute the reflected and transmitted wave. The glass window has the thickness  $2a$ .

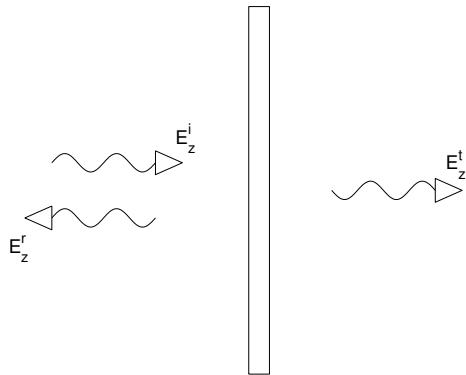


Figure 1: Glass window of thickness  $2a$  with an incident field  $E_z^i$ , the reflected field  $E_z^r$  and the transmitted field  $E_z^t$ .

We have the material parameters  $\epsilon(x)$ ,  $\mu(x) = \mu_0$  and  $\sigma(x)$  in the glass, where  $-a \leq x \leq a$ . The medium outside the window is air with  $\epsilon(x) = \epsilon_0$ ,  $\mu(x) = \mu_0$  and  $\sigma = 0$  for  $|x| > a$ . The total electric field satisfies the differential equation:

$$-\frac{d^2 E_z(x)}{dx^2} + \mu_0 [j\omega\sigma(x) - \omega^2\epsilon(x)] E_z(x) = 0 \quad (1)$$

## 2 Assignments

Here, we introduce some of the techniques used in electromagnetic scattering problems. One such technique is to formulate a boundary condition that “injects” the incoming wave by matching an expression for the incoming wave to the numerical solution in the air region. The matching is done in the air outside the scatterer, where the incoming field is known analytically. In addition, the boundary condition should be constructed such that the reflected wave (and the transmitted wave) is “received” by the same boundary condition and, thus, appear to continue to propagate in the infinite air-region outside the computational region. Again, we rely on that the reflected wave (and transmitted wave) is known analytically in the air region. Following this procedure for our 1D problem, we can do the matching at two points  $x = \pm b$  where the discretized solution in the computational domain  $|x| < b$  is related to the fields outside this region by means of the boundary conditions. Here, we need to have  $b > a$ , so that the matching points are in the air.

## 2.1 Formulate boundary condition

The first task is to derive the appropriate boundary conditions analytically for the two free-space regions: (i) the region to the left of the dielectric plate described by  $x < -a$ ; and (ii) the region to the right of the dielectric plate described by  $x > a$ .

Let the incident field be  $E_z^i(x) = E_0 \exp(-jk_0x)$ , which is useful in the region  $x < -a$  only. Introduce the reflected field as  $E_z^r(x) = E_r \exp(+jk_0x)$ , which is also useful in the region  $x < -a$  only. Also, introduce the transmitted field as  $E_z^t(x) = E_t \exp(-jk_0x)$ , which is useful in the region  $x > a$  only. You can use Eq. (1) to get  $k_0 = \omega/c_0$  where  $c_0 = 1/\sqrt{\epsilon_0\mu_0}$ .

What is a priori known and unknown in the expressions above? How can this information be used to formulate the appropriate boundary conditions at  $x = -b$  and  $x = b$ , respectively? The boundary condition should involve the total electric field  $E_z(x)$  and its first derivative only. (Note that  $b$  is quite arbitrary as long as it is larger than  $a$ .)

Note that it is important to work with the region  $x < -a$  and the region  $x > a$  separately. Here are some practical hints on how to proceed:

1. Write down the expression for the total electric field (by means of superposition if needed)
2. Differentiate the total electric field with respect to  $x$
3. Use the two equations (from step 1 and 2 above) to eliminate the unknown field (i.e. the reflected field or the transmitted field), which gives an equation that is the sought boundary condition
4. Check that the only unknown quantity in the boundary condition is the (sought) total electric field and, thus, that all other quantities are known

## 2.2 Generate grid and system matrix

We use two different grids:

**G1** The first grid is chosen such that the material interfaces  $x = \pm a$  fall in-between grid points. We use the grid points  $x_n = (n + \frac{1}{2})\Delta x$  with  $\Delta x = 2a/N$ , an even integer  $N \geq 4$  and  $n = -N - 1, -N, \dots, N$ .

**G2** The second grid is chosen such that the material interfaces  $x = \pm a$  fall on grid points. We use the grid points  $x_n = n\Delta x$  with  $\Delta x = 2a/N$ , an even integer  $N \geq 4$  and  $n = -N, -N + 1, \dots, N$ .

These grids discretize a region of (roughly) length  $a$  in each air region outside the glass window, where at least two grid points are placed in the air region.

Denote the unknowns on the grid by  $\zeta_n$ , i.e.  $E_z(x_n) = \zeta_n$ . Discretize the differential equation (1) and your boundary conditions using finite differences, both with an error that is proportional to  $h^2$ . The boundary condition involving no higher than first derivatives is best centered on the half-grid.

Using the boundary conditions and the differential equation, we have a system of linear equations  $\mathbf{Az} = \mathbf{b}$  to solve, where  $\mathbf{z} = [\zeta_1, \zeta_2, \dots, \zeta_{N_{gp}}]^T$  and  $N_{gp}$  is the

number of grid points. Write down the matrix  $\mathbf{A}$  and the right hand side  $\mathbf{b}$  in the special case when  $N = 4$  for the discretization G1. Follow the same procedure for the discretization G2. What are the similarities and differences when you compare the discretization G1 and the discretization G2? What may the implications be and how can you handle this?

Find a way of computing the reflection and transmission coefficients from the numerical solution.

## 2.3 Numerical implementation

Implement your numerical algorithm in MATLAB for an arbitrary  $N$  and both discretizations G1 and G2.

## 2.4 Numerical tests

Test your implementation on the case when the glass window has constant relative permittivity  $\epsilon_r$  and conductivity  $\sigma$ . The reflection and transmission coefficient can be calculated analytically in this case and they are given by:

$$\begin{aligned} R &= \frac{(k_0^2 - k_1^2)}{\Delta} e^{j2ak_0} (e^{j4ak_1} - 1) \\ T &= \frac{k_0 k_1}{\Delta} 4 e^{j2a(k_0 + k_1)} \end{aligned} \tag{2}$$

where  $\Delta = (k_0 + k_1)^2 e^{j4ak_1} - (k_0 - k_1)^2$ ,  $k_0 = \omega/c_0$  and  $k_1 = \sqrt{\epsilon_r k_0^2 - j\omega\mu_0\sigma}$ .

Use the thickness  $a = 2$  cm in combination with the constant material parameters  $\epsilon_r = 2.5$  and  $\sigma = 0.02$  S/m.

For the frequency  $\omega = 3 \cdot 10^9$  rad/s, compute  $R$  and  $T$  numerically on the discretization G1 for a set of appropriately chosen values of  $N$ . Do the numerically computed values of  $R$  and  $T$  converge towards the analytical values? Which order of convergence do you find?

### 2.4.1 Optional problems

These problems give credit points if they are correctly solved.

#### 5 credit points

Now repeat the above test for the discretization G2. Did this change the convergence properties? If so, why? By the way, how do you choose  $\epsilon(\pm a)$ ?

#### 5 credit points

Also, compute  $R$  and  $T$  as functions of frequency between 0.1 and 10 GHz, where you should use both the discretization G1 and G2 with a fixed value of  $N$ . How do the solutions compare? How does the error change with respect to the frequency? Explain your findings.

**5 credit points**

Compute  $R$  and  $T$  as a function of frequency between 0.1 and 10 GHz for an inhomogeneous window in the region  $|x| \leq a$  with the material parameters:

$$\begin{aligned}\sigma(x) &= 0.02p(x) \\ \epsilon(x) &= \epsilon_0 [1 + 5p(x)]\end{aligned}$$

where

$$p(x) = 1 - \left(\frac{x}{a}\right)^2$$

is a parabolic profile with  $p(\pm a) = 0$ .